

# Nanotube mechanical resonators with quality factors of up to 5 million

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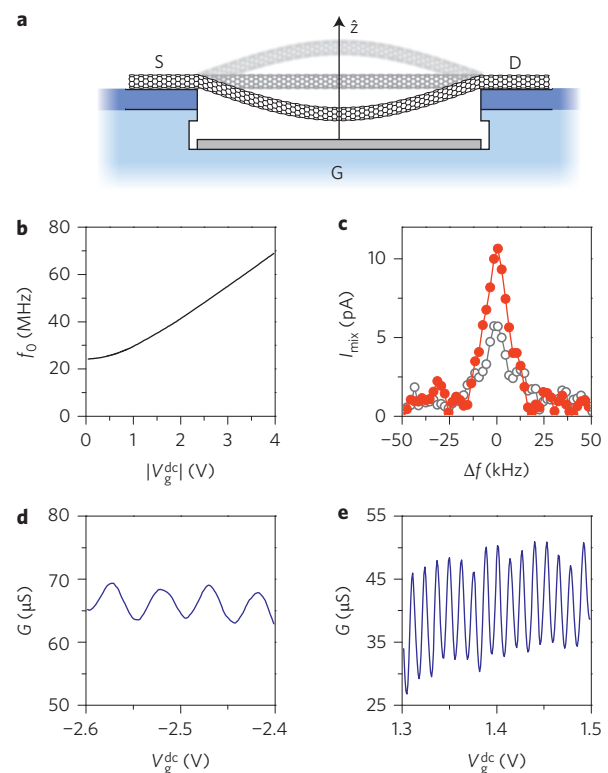
**Carbon nanotube mechanical resonators have attracted considerable interest because of their small mass, the high quality of their surfaces, and the pristine electronic states they host<sup>1–4</sup>. However, their small dimensions result in fragile vibrational states that are difficult to measure. Here, we observe quality factors  $Q$  as high as  $5 \times 10^5$  in ultra-clean nanotube resonators at a cryostat temperature of 30 mK, where we define  $Q$  as the ratio of the resonant frequency over the linewidth. Measuring such high quality factors requires the use of an ultra-low-noise method to rapidly detect minuscule vibrations, as well as careful reduction of the noise of the electrostatic environment. We observe that the measured quality factors fluctuate because of fluctuations of the resonant frequency. We measure record-high quality factors, which are comparable to the highest  $Q$  values reported in mechanical resonators of much larger size<sup>5,6</sup>, a remarkable result considering that reducing the size of resonators is usually concomitant with decreasing quality factors. The combination of ultra-low mass and very large  $Q$  offers new opportunities for ultra-sensitive detection schemes and quantum optomechanical experiments.**

In recent years, endeavours to boost quality factors in nano- and micromechanical resonators have been stimulated by the need to develop innovative approaches to sensing<sup>7</sup>, signal processing<sup>8</sup> and quantum physics<sup>9</sup>. Strategies to enhance quality factors have proceeded along three main routes. First, the quality of the host material has been improved. To this end, new materials have been employed, such as high-tensile-stress silicon nitride membranes<sup>5,10</sup> and single-crystal diamond films<sup>11</sup>. In addition, surface friction has been lowered by optimizing fabrication processes and reducing contamination<sup>12</sup>. Second, schemes to isolate the resonator from its surrounding environment have been developed, based on new resonator layouts<sup>13,14</sup> and on optical trapping of thin membranes and levitated particles<sup>15,16</sup>. Third, and most straightforwardly,  $Q$ -factors have been improved by operating resonators at cryogenic temperatures<sup>17</sup>.

Schemes to enhance  $Q$ -factors in nanotube resonators have focused on reducing contamination by growing ultra-clean nanotubes and by cooling resonators down to millikelvin temperatures<sup>2</sup>. Even though  $Q$ -factors, measured from the linewidth of driven resonances, have been improved up to  $\sim 1.5 \times 10^5$ , they are still much lower than the values routinely obtained with larger resonators fabricated from bulk materials using top-down techniques<sup>6</sup>. This result is somewhat disappointing, because the high crystallinity of nanotubes and their lack of dangling bonds at the surface are expected to minimize the surface friction that limits the  $Q$ -factor in some nanomechanical systems<sup>18</sup>.

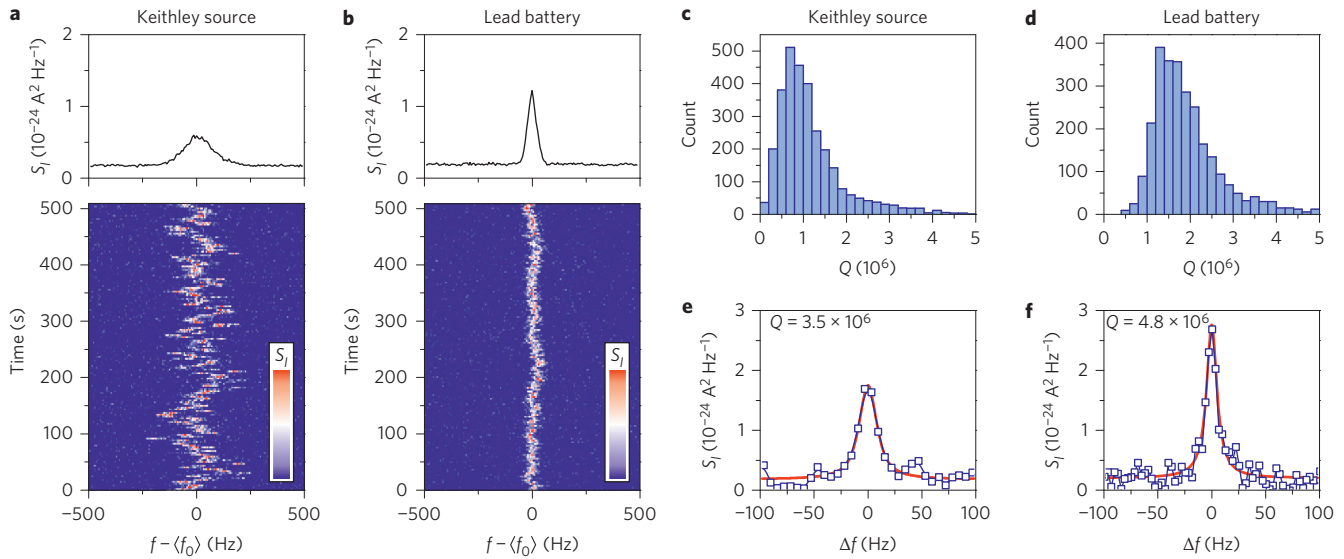
Here, we find that the actual values of the  $Q$ -factors can be significantly higher than hitherto appreciated, but that revealing these values requires improving the measurement technique.

Namely, the dynamics of the nanotube has to be captured in a regime of vanishingly small displacement in order to minimize non-linear effects. In addition, noise from the electrostatic environment has to be reduced as much as possible. Indeed, owing to the ultra-small mass of nanotubes, this electrostatic noise affects the frequency of the nanotube resonator enormously and broadens the



**Figure 1 | Carbon nanotube mechanical resonator.** **a**, Schematic of device. The nanotube is contacted by source (S) and drain (D) electrodes, and is suspended over a gate electrode (G). The trench has a width of 1.8  $\mu$ m and a depth of  $\sim 350$  nm. **b**, Resonant frequency  $f_0$  as a function of gate voltage  $|V_g^{dc}|$  for the lowest-lying mechanical mode. **c**, Mixing current  $I_{mix}$  as a function of drive frequency  $\Delta f$  (measured from  $f_0 = 44.1$  MHz), using the FM technique.  $V_g^{dc} = -2.2$  V. Two different driving voltage amplitudes were used: 13  $\mu$ V (filled red circles) and 8  $\mu$ V (open circles). A lock-in amplifier with a time constant of 300 ms was used. In the FM technique, the  $Q$ -factor is extracted from the width of the foot of the resonance<sup>20,21</sup>, yielding  $Q \approx 1,700$ . **d,e**, Conductance  $G$  as a function of  $V_g^{dc}$ , in the Fabry-Perot regime (**d**) and in the Coulomb blockade regime (**e**). The full  $G(V_g^{dc})$  trace is shown in Supplementary Section I.

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**Figure 2 | Fluctuations of the Q-factor and resonant frequency.** **a**, Bottom: Power spectra of current fluctuations  $S_f(f - \langle f_0 \rangle)$  acquired successively in time, using a commercial d.c. voltage source (Keithley) to supply the gate voltage ( $V_g^{\text{dc}} = -3.037$  V). For each of these spectra the measurement time was 3.2 s. Top: Resonance obtained by averaging all spectra. **b**, Same experiment as in **a**, this time using a lead battery to supply the gate voltage. Scale bars: power spectral density  $S_f = 0.15 \times 10^{-24} \text{ A}^2 \text{ Hz}^{-1}$  (blue) to  $S_f = 2.50 \times 10^{-24} \text{ A}^2 \text{ Hz}^{-1}$  (red). **c,d**, Histograms of Q-factor using the Keithley source (**c**) and the lead battery (**d**), constructed from 3,000 power spectra acquired with the same settings as in **a,b**. **e,f**, Examples of high Q resonances obtained with the Keithley source (**e**) and the lead battery (**f**). Red curves are fits to Lorentzian functions. For all panels,  $\langle f_0 \rangle = 55.6$  MHz is the time-averaged resonant frequency.

mechanical linewidth. All these experimental requirements make it challenging to unmask the intrinsic Q-factor. Progress in measuring ring-down with nanotubes has been made<sup>19</sup>, but it has not revealed higher Q-factor values. One reason for this might be that the large displacements in those measurements lead to sizeable nonlinearities.

The geometry of our device, as well as its characterization, are presented in Fig. 1. The nanotube is contacted by source (S) and drain (D) electrodes, and is suspended over a trench; at the bottom of the trench is a local gate electrode (Fig. 1a). In this scheme, the ultra-clean nanotube was grown by chemical vapour deposition in the last step of the fabrication process of the resonator, making it free of fabrication residues. The device was cooled to 30 mK, at which temperature all the data presented here were taken. We identified the lowest-lying flexural mode of the resonator using the frequency-modulated (FM) mixing technique<sup>20,21</sup>, and studied its dependence on gate voltage  $|V_g^{\text{dc}}|$  (Fig. 1b). Figure 1c presents resonance lineshapes in response to oscillating electrostatic forces (measured with the FM technique), which yield  $Q = 1,700$ . The voltages used to produce these driving forces were kept low so that the resonance lineshapes were just above the noise floor.

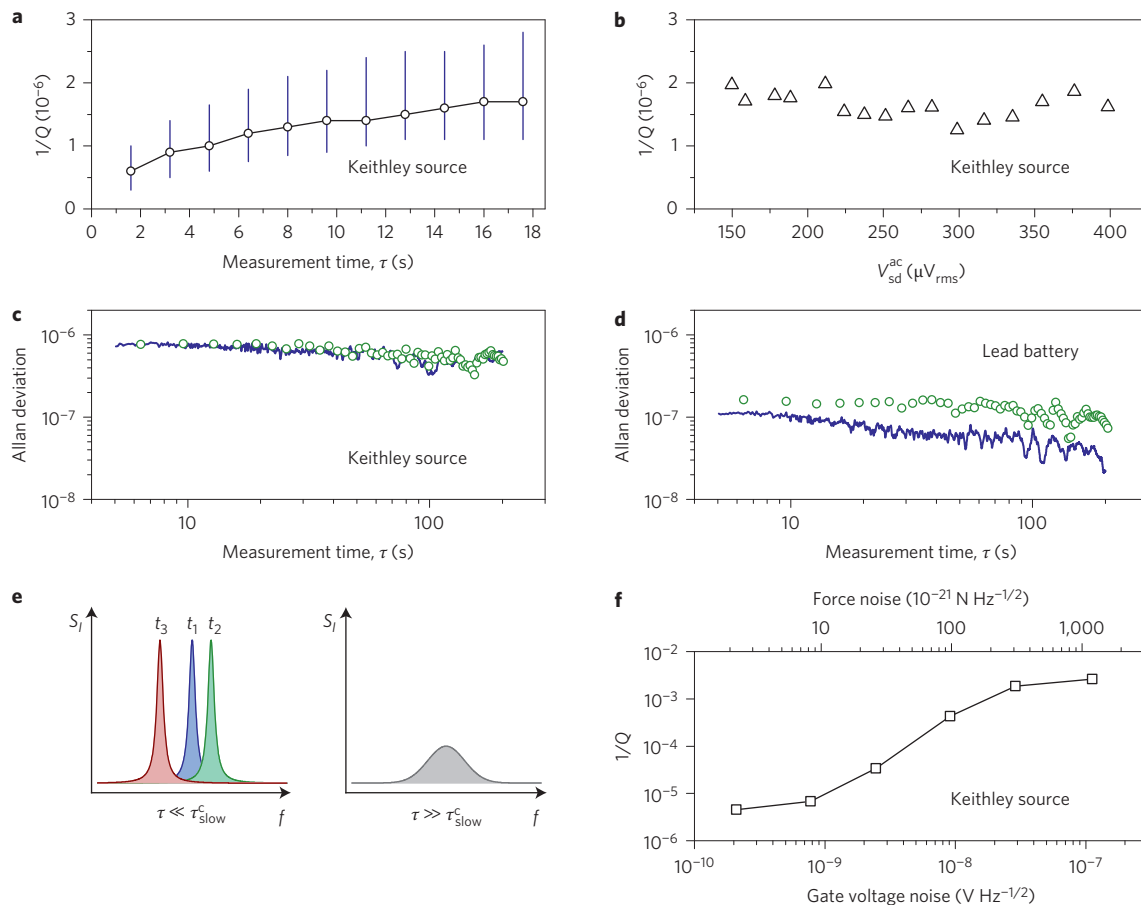
An ultra-sensitive detection method (described in ref. 22) was used to capture the tiny amplitude of the thermal vibrations at 30 mK. In contrast to the FM technique, the resonator was not driven by an oscillating force. Displacement fluctuations were transduced into current fluctuations, from which power spectra  $S_f$  were measured (see Methods). We operated the resonator within the electron Fabry–Perot regime (Fig. 1d), where the effect of electron transport on mechanical vibrations is less pronounced than in the Coulomb blockade regime (Fig. 1e)<sup>2–4,23</sup>. A typical resonance lineshape, obtained by averaging power spectra for  $\sim 512$  s, is shown in the upper panel of Fig. 2a. The corresponding Q-factor is  $Q \approx 4 \times 10^5$  for a resonant frequency  $f_0 = 55.6$  MHz. Remarkably, such a Q-factor is 200 times higher than that measured with the FM mixing technique (Fig. 1c).

We find that both the Q-factor and  $f_0$  fluctuate in time. To show this, spectra obtained over a measurement time  $\tau = 3.2$  s were acquired successively, using either a commercial Keithley source

or a simple lead battery to supply  $V_g^{\text{dc}}$  (see colour plots of  $S_f$  as a function of frequency and time in Fig. 2a,b). Frequency fluctuations with the Keithley source are larger than with the lead battery. The Q-factor also fluctuates, and its distribution is broad and asymmetric (Fig. 2c,d). On average, Q-factors are higher with the lead battery than with the Keithley source. Although fluctuations in  $f_0$  have been observed in high-Q mechanical resonators<sup>24–26</sup>, fluctuations in the measured Q-factor have not been discussed thus far. We show in the following that both fluctuations are closely related.

The averaged Q-factor decreases with measurement time (Fig. 3a). Once the measurement time is set, the Q-factor does not reveal any marked dependence on the amplitude  $V_{\text{sd}}^{\text{ac}}$  of the oscillating source–drain bias used to read out current fluctuations (Fig. 3b). This shows that  $V_{\text{sd}}^{\text{ac}}$  does not affect the measured motion of the resonator. For example, if the resonator were to heat up due to Joule heating, the Q-factor would decrease as  $V_{\text{sd}}^{\text{ac}}$  increases, and if the resonator were to self-oscillate, the Q-factor would vary as  $V_{\text{sd}}^{\text{ac}}$  increases. Neither the Q-factor nor  $f_0$  changes as  $V_g^{\text{dc}}$  is swept through a conductance oscillation (Supplementary Section VI). This confirms that the effect of electron transport on the vibrations is weak. This is crucial to our experiment, because Coulomb blockade would reduce the Q-factor<sup>2–4,23</sup>.

The observed frequency fluctuations are associated with the electrostatic noise of the environment. In the case of the Keithley source, frequency fluctuations are traced back to the voltage fluctuations of the source itself as a result of the strong gate voltage dependence of  $f_0$ . To show this, we transformed voltage fluctuations into Allan deviation  $\sigma_A$  using the  $f_0$ -to- $V_g^{\text{dc}}$  conversion factor measured in Fig. 1b,  $\sim 1.4 \times 10^7 \text{ Hz V}^{-1}$  (see Methods). In Fig. 3c we find that the measured Allan deviation of the resonant frequency of the nanotube (green open circles) coincides with the Allan deviation expected from the gate voltage fluctuations generated by the source (blue trace). The frequency noise is of  $1/f$ -type (pink noise), because  $\sigma_A$  is essentially constant as a function of measurement time  $\tau$ . By contrast, the lead battery is stable enough that it does not significantly affect  $f_0$ . The Allan deviation expected from the voltage fluctuations of the lead battery is smaller than  $\sigma_A(\tau)$  measured with the nanotube resonator (Fig. 3d). The origin of the



**Figure 3 | Characterization of the Q-factor and of the fluctuations in  $f_0$ .** **a**,  $1/Q$  as a function of measurement time  $\tau$ , using the Keithley source. For each measurement time, 300 power spectra were acquired and a histogram of  $1/Q$  was built. Circles denote  $1/Q$  at the maximum of the histograms and bars represent the full-width at half-maximum of the histograms. The resonant frequency is  $f_0 = 55.6$  MHz for **a-d**. **b**,  $1/Q$  as a function of  $V_{sd}^{ac}$  for  $\tau = 16$  s. **c,d**, Allan deviation of  $f_0$  as a function of  $\tau$  with the Keithley source (**c**) and with the lead battery (**d**). Green circles indicate measured resonant frequencies and blue traces represent resonant frequencies estimated from gate voltage fluctuations. **e**, Schematic of resonance lineshapes for short (left) and long (right) measurement times  $\tau$  compared to the characteristic time of the slow frequency noise  $\tau_{slow}^c$ .  $t_{1,2,3}$  are three successive instants. **f**,  $1/Q$  as a function of added gate voltage noise at  $V_g^{dc} = -2.2$  V ( $f_0 = 44.1$  MHz) for  $\tau = 16$  s. The gate voltage noise was applied using the Johnson-Nyquist noise of a 50  $\Omega$  resistor at room temperature amplified by different gains. It creates a white electrostatic force noise between the nanotube and the gate (top axis).

observed frequency fluctuations with the lead battery is not clear. Because  $\sigma_A$  remains constant as a function of  $\tau$  ( $1/f$  noise),  $f_0$  fluctuations might be related to two-level systems such as charge fluctuators in the gate dielectric.

The Q-factor is also affected by the electrostatic noise of the environment. This can be inferred from a comparison of Fig. 2a and b. Larger fluctuations of the resonant frequency (lower panels) result in a larger resonance linewidth (upper panels), and hence a lower Q-factor.

The fluctuations of the quality factor, the asymmetry of its distribution and its dependence on measurement time are all attributed to the fluctuations of the resonant frequency. To show this, we separated this frequency noise into a slow part and a fast part on the scale of the ring-down time (see Methods and Supplementary Section X). For a measurement time  $\tau$  that is short compared to the characteristic timescale of the slow frequency noise  $\tau_{slow}^c$ , resonances have a Lorentzian lineshape with a constant width  $2\tilde{\Gamma}$  and a resonant frequency that fluctuates from one measurement to the next. For  $\tau \gg \tau_{slow}^c$ , resonances are broadened by the time average of many such Lorentzians, resulting in non-Lorentzian lineshapes (Fig. 3e). For  $\tau \approx \tau_{slow}^c$ , linewidths are larger than  $2\tilde{\Gamma}$ , and fluctuate from one measurement to the next. On increasing  $\tau$ , linewidths tend to increase because the resonator has time to explore a larger

frequency range. The distribution of linewidths is asymmetric because linewidths have a fixed lower bound given by  $2\tilde{\Gamma}$  (Supplementary Section X).

Figure 2e,f presents two high-Q resonance lineshapes (obtained with both gate voltage sources), which give values of  $Q = 3.5 \times 10^6$  (Keithley source) and  $Q = 4.8 \times 10^6$  (lead battery). We verified that the areas of the resonances in the  $S_I$  spectra in Fig. 2e,f are equal (within 10%) to the areas of the averaged resonances in Fig. 2a,b. This confirms that these sharp resonances do capture the dynamics of the nanotube, in spite of the relatively low number of measurement points dictated by the short measurement time. A slightly lower quality factor is obtained in an additional device, also operated in the Fabry-Perot regime (Supplementary Section IX), confirming the robustness of high-Q resonances. These Q-factors are comparable to the highest values measured in large micromechanical resonators<sup>5</sup>. Yet, they may still be limited by the measurement and may not have reached the intrinsic Q-factor of nanotube resonators, defined as  $f_0$  multiplied by the small-amplitude ring-down time (the ring-down time is not known, but it is smaller than  $\tau$ ; Supplementary Section X).

The large quality factors observed here are associated with the small amplitude of the nanotube vibrations. Using the equipartition theorem, the mode temperature is obtained as  $T = 44 \pm 10$  mK,

which corresponds to a phonon population of  $n = k_B T / h f_0 = 16 \pm 4$ , where  $k_B$  is the Boltzmann constant and  $h$  is Planck's constant (Supplementary Section V). In this estimate, we use the areas of the resonances in Fig. 2, which are all equal within 10%. From the temperature, we calculate that the variance of displacement is  $\sim (35 \text{ pm})^2$ .

Larger displacements translate into lower  $Q$ -factors. This is illustrated in Fig. 3f, where a white voltage noise is applied to the gate electrode to enhance the displacement. Possible origins of this behaviour could be associated with nonlinear damping forces, which result in a mechanical linewidth that depends on the amplitude of motion and the spectral broadening of the resonance, which is induced by the combination of nonlinear conservative forces and displacement fluctuations<sup>21,27–29</sup>. Note that the applied voltage noise also induces fluctuations in  $f_0$ , but their contribution to the measured resonance linewidth is negligible (Supplementary Section VII). The temperature dependence of the  $Q$ -factor could not be measured in our current measurement set-up.

The giant quality factors and the associated weak fluctuations of  $f_0$  hold promise for diverse sensing experiments. The limit to force sensing is ultimately set by the force noise  $S_f = 8\pi M k_B T f_0 / Q$  (ref. 22). Using  $M = 4.4 \times 10^{-21} \text{ kg}$ ,  $Q = 4.8 \times 10^6$  and  $T \approx 44 \text{ mK}$ , we obtain  $\sqrt{S_f} \approx 1 \times 10^{-21} \text{ N Hz}^{-1/2}$ , which is lower than what has been achieved with mechanical resonators to date<sup>22</sup>. The sensitivity of mass sensing and force gradient detection is given by the Allan deviation of frequency fluctuations ( $\delta f_0 \approx 8 \text{ Hz}$  for  $\tau \approx 6 \text{ s}$ ) in Fig. 3d obtained with the lead battery. The latter translates into a mass resolution of  $\delta M = 2M \times \delta f_0 / f_0 \approx 1 \times 10^{-27} \text{ kg}$ , which is as good as the best estimates on record<sup>1</sup>. We extract a force gradient resolution of  $8\pi^2 M f_0 \delta f_0 \approx 1 \times 10^{-10} \text{ N m}^{-1}$ , which compares favourably with the best values reported thus far<sup>30</sup>.

Nanotube resonators are relevant candidates for exploring the quantum regime of nanomechanics. Their low mass leads to large zero-point motion,  $\sqrt{\hbar / (4\pi f_0 M)} \approx 6 \text{ pm}$  and allows the coupling to other quantum systems to be enhanced. High  $Q$ -factors are necessary for the quantum manipulation of mechanical states. In an experiment where the resonator is cooled to the ground state with passive feedback, the lifetime of the ground state is  $\tau_{\text{ph}} = \hbar Q / k_B T \approx 1 \times 10^{-3} \text{ s}$  (for  $k_B T > h f_0$ ) using  $T \approx 44 \text{ mK}$  and assuming that  $Q = 4.5 \times 10^6$  is related to the ring-down time. Our nanotube resonator demonstrates  $Q f_0 = 3 \times 10^{14} \text{ Hz}$ , which compares well with the highest values measured to date in nano- and micromechanical resonators<sup>14,31</sup>.

Overall, our work shows that the  $Q$ -factor of ultra-clean nanotube resonators can reach very high values, provided that the resonators are cooled to a low enough temperature for nonlinear effects to be negligible, that slow frequency noise is reduced, that measurement times are short and that the effect of coupling between vibrations and Coulomb blockade is suppressed. The unique combination of ultra-low mass and giant quality factors offers new opportunities for ultra-sensitive detection schemes and optomechanical experiments in the quantum regime.

## Methods

**Detecting thermal vibrations.** We used an ultra-sensitive detection method that allowed us to capture the tiny amplitude of the thermal vibrations in a dilution refrigerator cooled to 30 mK. Displacement fluctuations  $\delta z$  in direction  $\hat{z}$  normal to the gate were transduced into conductance fluctuations  $\delta G = \frac{dG}{dV_g} \frac{dV_g}{dC_g} \delta z$ , where  $C_g$  is the capacitance between the nanotube and the gate, and  $C_g' = dC_g / dz$  (for the estimation of  $C_g'$ , see Supplementary Section II). Large transduced signals require a large transconductance  $dG/dV_g$ . The largest transconductance was obtained in the Coulomb blockade regime, for  $V_g^{\text{dc}} > 0$  (Fig. 1e), as is usually observed in ultra-clean suspended nanotubes<sup>32</sup>. However, Coulomb blockade reduces  $Q$ -factors, because it amplifies the coupling between electron transport and mechanical vibrations<sup>2–4,23</sup>. For this reason, we operated the resonator within the Fabry–Perot regime, realized for  $V_g^{\text{dc}} < 0$ , even though  $dG/dV_g$  is lower (Fig. 1d). In this regime, oscillations in conductance originate from quantum interferences of electronic waves, and the effect of the coupling between vibrations and Coulomb blockade is weaker. The tiny

conductance fluctuations  $\delta G$  are parametrically downconverted into low-frequency current fluctuations  $\delta I$  by applying a small oscillating voltage of amplitude  $V_{\text{sd}}^{\text{ac}}$  across source and drain, at a frequency  $f_{\text{sd}}$  shifted by  $\sim 10 \text{ kHz}$  from the mechanical resonant frequency  $f_0$ . Power spectra  $S_I$  of fluctuations  $\delta I$  were measured at frequencies  $|f_{\text{sd}} - f_0| \approx 10 \text{ kHz}$  with a cross-correlation technique using a vector signal analyser<sup>22</sup>.

**Allan deviation.** We calculate the Allan deviation  $\sigma_A$  as

$$\sigma_A^2(\tau) = \frac{1}{2(N-1)} \sum_{i=1}^{N-1} \left( \frac{\langle f_{i+1} \rangle_\tau - \langle f_i \rangle_\tau}{\langle f_0 \rangle} \right)^2$$

where  $\langle f_{i+1} \rangle_\tau$  and  $\langle f_i \rangle_\tau$  are two subsequent measurements of  $f_0$  averaged over the measurement time  $\tau$ ,  $N$  is the number of averaged frequency measurements and  $\langle f_0 \rangle$  is the average of  $f_0$  over the whole measurement<sup>33</sup>. We define  $f_0$  as the frequency for which  $S_I$  is largest.

**Power spectrum of displacement and frequency noise.** We separated the frequency noise into a slow part and a fast part on the scale of the ring-down time. The power spectrum of displacement  $S_q$  (which is proportional to  $S_I$ ) as a function of angular frequency  $\omega = 2\pi f$  is given by

$$S_q(\omega) = \frac{k_B T}{M \omega_0^2} \frac{1}{\tau} \int_0^\tau dt \frac{\tilde{\Gamma}}{\tilde{\Gamma}^2 + [\omega - \tilde{\omega}_0 - \xi_{\text{slow}}(t)]^2}$$

where  $k_B$  is the Boltzmann constant,  $T$  is the mode temperature,  $t$  is the time and  $M$  is the modal mass.  $\tilde{\Gamma}$  is the sum of the reciprocal ring-down time and of the broadening due to fast frequency noise,  $\tilde{\omega}_0$  is the resonant angular frequency renormalized by the fast frequency noise and  $\xi_{\text{slow}}$  is the slow part of the frequency noise (Supplementary Section X). The area  $\int_0^\tau S_q(\omega) d\omega = \pi k_B T / M \omega_0^2$  is given by the equipartition theorem, so it is independent of frequency noise.

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### Author contributions

J.M. developed the experimental set-up, carried out the measurements and analysed the data. A.E. fabricated the devices. J.G. provided support for the experimental set-up. M.I.D. and A.B. provided support for the analysis. M.I.D. wrote Supplementary Section X. J.M., M.I.D. and A.B. wrote the manuscript, with critical comments from all authors. A.B. and J.M. conceived the experiment. A.B. supervised the work.

### Additional information

Supplementary information is available in the [online version](#) of the paper. Reprints and permissions information is available online at [www.nature.com/reprints](http://www.nature.com/reprints). Correspondence and requests for materials should be addressed to A.B.

### Competing financial interests

The authors declare no competing financial interests.

# Nanotube mechanical resonators with quality factors of up to 5 million

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## I. CONDUCTANCE AS A FUNCTION OF GATE VOLTAGE

The conductance  $G$  as a function of gate voltage  $V_g^{DC}$  at 30 mK is shown in Supplementary Fig. S1. The regime for positive  $V_g^{DC}$  corresponds to Coulomb blockade (Supplementary Fig. S1b, middle and right-hand-side panels). Indeed, the length of the blockaded region, estimated to be  $\sim 1.5 \mu\text{m}$  from the separation between conductance oscillations, is close to the width of the trench (see next section). For negative  $V_g^{DC}$ , charge transport is in the so-called Fabry-Perot regime (Supplementary Fig. S1b, left-hand-side panel). The period in  $V_g^{DC}$  of the oscillations of  $G$  is a few times larger than the period of oscillations for positive  $V_g^{DC}$ , as usually observed for suspended nanotubes. In addition, the conductance is close to  $2e^2/h$ , indicating that the electronic transmission of each contact is high.

The measurement shown in Supplementary Fig. S1 is typical of ultra-clean nanotubes [1]. The regions of the nanotube near the metal electrodes remain  $p$ -doped, due to the work function of the electrodes, whereas the suspended part of the nanotube can be doped with electrons or holes using  $V_g^{DC}$ . For positive  $V_g^{DC}$ ,  $p-n$  junctions are formed near the metal electrodes, resulting in a Coulomb blockaded region along the suspended nanotube. For negative  $V_g^{DC}$ , the nanotube is  $p$ -doped along the whole tube and no tunnel barriers are formed. Near  $V_g^{DC} = 0$ , the conductance is zero because the Fermi energy lies inside the energy band gap along the entire suspended part of the nanotube.

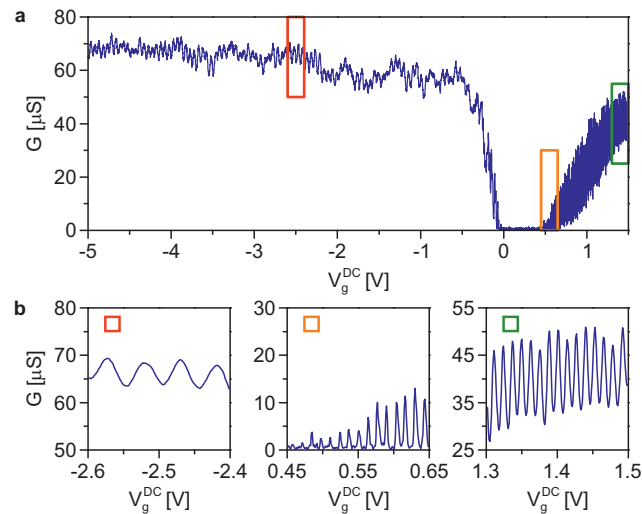


Figure S1. (a) Conductance  $G$  as a function of gate voltage  $V_g^{DC}$ . Regions within colored rectangles are blown up in (b).

## II. ESTIMATING $C'_g$

We estimate the capacitance  $C_g$  between the nanotube and the gate from the separation  $\Delta V_g^{DC} = 13 \pm 1$  mV between two conductance peaks in the Coulomb blockade regime (Supplementary Fig. S1b, central and right-hand-side panels):  $C_g = e/\Delta V_g^{DC} = 1.2 \pm 0.1 \times 10^{-17}$  F. This value is close to the model capacitance between a cylinder of length  $L$  and radius  $r$ , and a plane a distance  $h$  away:

$$C_g = \frac{2\pi\epsilon_0 L}{\ln\left(\frac{2(h-z)}{r}\right)},$$

where  $\epsilon_0$  is the vacuum permittivity,  $h$  is the separation between the nanotube and the gate, and  $z \ll h$  is a small displacement of the cylinder in the direction normal to the gate. The derivative  $dC_g/dz$  reads

$$C'_g = \left(\frac{dC_g}{dz}\right)_{z=0} = \frac{C_g}{h \ln(2h/r)} = (5.2 \pm 1.9) \times 10^{-12} \text{ F/m},$$

using  $h = 350 \pm 50$  nm and  $r = 1 \pm 0.5$  nm (the typical radius of nanotubes obtained with our chemical vapour deposition technique).

## III. ESTIMATING THE EFFECTIVE MASS

We study the fundamental flexural mode of the nanotube resonator (see Fig. 1b of the main text). We use a simple model whereby the nanotube is straight and is perpendicular to the trench. The effective mass  $M$  of the mode is related to the mass of the nanotube  $M_{NT}$  as

$$M = M_{NT} \frac{1}{L} \int_0^L [\phi(x)]^2 dx,$$

where  $L$  is the length of the nanotube and  $\phi(x)$  is the shape of the mode, which is normalized so that  $\max[\phi(x)] = 1$ . Given that mechanical tension is induced in the nanotube by the contacts and by the gate voltage, we assume that the modal shape is  $\phi(x) = \sin(\pi x/L)$ . The latter is the simplest approximation for the shape of a beam under tension. We emphasize that the expression for  $M$  takes into account the shape of the vibrational mode; all other quantities are measured with respect to the amplitude of this mode. To estimate  $M_{NT}$ , we also assume that the length of the nanotube is equal to the trench width ( $L = 1.8 \pm 0.2 \mu\text{m}$ )



and that  $r = 1$  nm as in Section II. Therefore

$$M = \frac{1}{2} \left( 2M_C \times \frac{2\pi r \times L}{A} \right) = (4.4 \pm 2.4) \times 10^{-21} \text{ kg},$$

where  $M_C = 2 \times 10^{-26}$  kg is the mass of a carbon atom and  $A = 5.2 \times 10^{-20}$  m<sup>2</sup> is the surface area of a hexagon in the honeycomb lattice of graphene.

#### IV. ORIENTATION OF THE MODE WITH RESPECT TO THE GATE ELECTRODE

The orientation of the vibrations of the eigenmode depends on the static curvature of the suspended nanotube, which builds in during the fabrication of the resonator. Since the static curvature cannot be controlled and cannot be accurately measured, the eigenmode can vibrate in any direction. For a real nanotube, the displacement along the nanotube can be quite complicated. However, we will use a simplified model where at least for the lowest mode the displacement is in one plane. We will characterize this plane by the angle  $\theta$  it makes with the plane parallel to the surface of the gate electrode (Supplementary Fig. S2a).

We assume that current fluctuations  $\delta I$  at the drain electrode are proportional to motional fluctuations  $\delta z$  along the direction  $\hat{z}$  normal to the gate electrode. Then, the current at the frequency close to the difference between the mode eigenfrequency and the frequency of the source-drain voltage is

$$\delta I = \beta \delta z = \frac{1}{2} \frac{dG}{dV_g} V_g^{DC} V_{sd}^{AC} \frac{C'_g}{C_g} \delta z, \quad (\text{S1})$$

where  $dG/dV_g$  is the transconductance,  $V_g^{DC}$  is the static gate voltage, and  $V_{sd}^{AC}$  is the amplitude of the oscillating source-drain voltage. We assume that the mode is polarized along  $\hat{q}$ , as shown in Supplementary Fig. S2a; hence,  $\delta z$  is the projection along  $\hat{z}$  of the motional fluctuation  $\delta q$  along  $\hat{q}$ :

$$\delta z = \delta q \sin \theta, \quad (\text{S2})$$

where  $\theta$  is the angle between  $\hat{y}$  and  $\hat{q}$ . To estimate  $\theta$ , we subject the nanotube to a weak electrostatic force by applying a small oscillating voltage with amplitude  $\delta V_g^{AC}$  to the gate. The component of the force along  $\hat{z}$  is  $\delta F_z = C'_g V_g^{DC} \delta V_g^{AC}$ . The center of mass of the nanotube experiences a force  $\delta F_q = \delta F_z \sin \theta$ , the projection of  $\delta F_z$  along  $\hat{q}$ . On resonance,

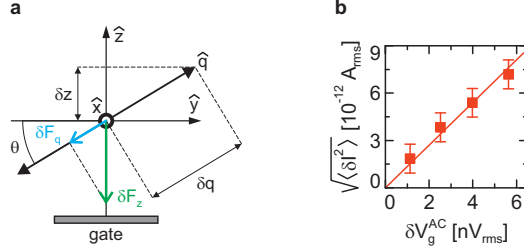


Figure S2. (a) Orientation of the displacement for a simple model of a straight nanotube parallel to the gate electrode.  $\hat{x}$  and  $\hat{y}$  are parallel to the gate, and  $\hat{z}$  is normal to the gate. The displacement (that is, the mode polarization) is along  $\hat{q}$ . The force  $\delta F_z$  along  $\hat{z}$  acts on the motion of the nanotube through the force  $\delta F_q$ , its projection onto  $\hat{q}$ . The projection of displacement  $\delta q$  onto  $\hat{z}$  is  $\delta z$ . (b) Standard deviation of current  $\sqrt{\langle \delta I^2 \rangle}$  induced by a small oscillating gate voltage of amplitude  $\delta V_g^{AC}$  applied on resonance.  $\delta V_g^{AC}$  produces the force  $\delta F_z$  in (a).

the displacement  $\delta q$  induced by  $\delta F_q$  reads

$$\delta q = \frac{Q}{M\omega_0^2} \delta F_q, \quad (\text{S3})$$

where  $Q$  is the quality factor of the resonance,  $M$  the effective mass, and  $\frac{\omega_0}{2\pi}$  the resonant frequency. In turn, the displacement  $\delta q$  induces current oscillations of variance  $\langle \delta I^2 \rangle$  at the drain:

$$\sqrt{\langle \delta I^2 \rangle} = \beta \sin^2 \theta \frac{Q}{M\omega_0^2} C'_g V_g^{DC} \delta V_g^{AC} = p \delta V_g^{AC}. \quad (\text{S4})$$

Supplementary Fig. S2b shows  $\sqrt{\langle \delta I^2 \rangle}$  as a function of  $\delta V_g^{AC}$ , measured with the technique described in the main text and in Ref. [2]. The dependence of  $\sqrt{\langle \delta I^2 \rangle}$  on  $\delta V_g^{AC}$  is linear and extrapolates to zero in the limit of zero  $\delta V_g^{AC}$ , as expected from Eq (S4). We obtain  $\theta = 60^\circ \pm 25^\circ$  from the slope in Supplementary Fig. S2b, using  $|V_g^{DC}| = 2.2$  V,  $V_{sd}^{AC} = 3.17 \times 10^{-4}$  V,  $C_g = (1.2 \pm 0.1) \times 10^{-17}$  F,  $C'_g = (5.2 \pm 1.9) \times 10^{-12}$  F/m,  $M = (4.4 \pm 2.4) \times 10^{-21}$  kg,  $\omega_0/(2\pi) = 44.1 \times 10^6$  Hz,  $Q = 5 \times 10^5$ ,  $dG/dV_g = 6.4 \times 10^{-4}$  S/V, and  $p = (1.3 \pm 0.2) \times 10^{-3}$  A/V.

The estimation of  $\theta$  comes with a large uncertainty that mostly originates from the uncertainties in the estimations of  $C'_g$  and  $M$ . These uncertainties, however, have little impact on the estimation of the modal temperature  $T$ , which we present in Section V. Indeed, we show that  $T$  is proportional to  $M/(C'_g \sin \theta)^2$ , a quantity that we can estimate rather precisely from the measurement shown in Supplementary Fig. 2b. For this, we rewrite

Eq. (S4) as:

$$\frac{M}{(C'_g \sin \theta)^2} = \frac{1}{p} \left( \frac{1}{2} \frac{dG}{dV_g} (V_g^{DC})^2 V_{sd}^{AC} \frac{1}{C_g} \frac{Q}{\omega_0^2} \right). \quad (\text{S5})$$

Using the values given above, we calculate the right-hand-side of Eq. (S5) and obtain

$$\frac{M}{(C'_g \sin \theta)^2} = 205 \pm 40 \text{ kg} \cdot \text{m}^2/\text{F}^2.$$

We use this value to estimate  $T$  in Section V.

## V. MODE TEMPERATURE

Using Eqs. (S1) and (S2), the equipartition theorem yields

$$k_B T = M \omega_0^2 \langle \delta q^2 \rangle = M \omega_0^2 \frac{1}{(\beta \sin \theta)^2} \frac{1}{2\pi} \int_{-\infty}^{\infty} S_I(\omega) d\omega, \quad (\text{S6})$$

where  $\langle \delta q^2 \rangle$  is the variance of displacement along  $\hat{q}$ , and  $S_I(\omega)$  is the *two-sided* power spectral density of current fluctuations  $\delta I$ . To make contact with the experiment, we also express  $k_B T$  in terms of  $S_I(2\pi f)$ , where  $f = \frac{\omega}{2\pi}$  is the natural frequency:

$$k_B T = M \omega_0^2 \frac{1}{(\beta \sin \theta)^2} \int_0^{\infty} 2S_I(2\pi f) df, \quad (\text{S7})$$

where we used

$$\frac{1}{2\pi} \int_{-\infty}^{\infty} S_I(\omega) d\omega = \int_{-\infty}^{\infty} S_I(2\pi f) df = 2 \int_0^{\infty} S_I(2\pi f) df.$$

In Eq. (S7),  $S_I(2\pi f)$  is defined as

$$S_I(2\pi f) = \lim_{\tau \rightarrow \infty} \int_{-\tau/2}^{\tau/2} \langle \delta I(t) \delta I(0) \rangle \exp[-i(2\pi f + \omega_{sd} - \omega_0)t] dt, \quad (\text{S8})$$

where  $\tau$  is the measurement time,  $\omega_{sd}$  is the off-resonance angular frequency of the source-drain voltage, and  $\omega_0$  is the resonant angular frequency. Experimentally, we measure the *single-sided* power spectral density  $S_I^{\text{exp}}(2\pi f) = 2S_I(2\pi f)$ .

We estimate the mode temperature  $T$  from the power spectra in Figs. 2e,f of the main text. We obtain  $T \simeq 44 \pm 10$  mK, using the following parameters:  $|V_g^{DC}| = 3.037$  V,  $dG/dV_g = 8.5 \times 10^{-4}$  S/V,  $V_{sd}^{AC} = 4 \times 10^{-4}$  V,  $C_g = (1.2 \pm 0.1) \times 10^{-17}$  F,  $\omega_0/(2\pi) = 55.6 \times 10^6$  Hz, and  $\int_0^{\infty} S_I^{\text{exp}}(2\pi f) df = 4.5 \times 10^{-23}$  A<sup>2</sup>. We also use  $M/(C'_g \sin \theta)^2 = 205 \pm 40$  kg  $\cdot$  m<sup>2</sup>/F<sup>2</sup> obtained in Section IV.

We were not able to carry out a temperature dependence of  $\langle \delta z^2 \rangle$ . Connecting thermometry lines to the cryostat would generate electrical noise in our measurement, masking the mechanical resonance in the spectra.

## VI. DEPENDENCES OF THE RESONANT FREQUENCY AND THE $Q$ -FACTOR ON DC GATE VOLTAGE

Supplementary Fig. S3a shows the resonant frequency as a function of  $V_g^{DC}$  obtained by measuring the mixing current  $I_{mix}$  with the FM technique [3] as a function of  $V_g^{DC}$  and drive frequency  $f$ . The intensity of  $I_{mix}$  varies with  $V_g^{DC}$  because it is proportional to the transconductance. The resonant frequency  $f_0$  is linear in  $V_g^{DC}$ . Supplementary Fig. S3c shows the inverse of the  $Q$ -factor as  $V_g^{DC}$  is stepped from the bottom of an oscillation in  $I^{DC}(V_g^{DC})$  to the top of this oscillation. No variation of  $1/Q$  is seen.

The dependences of  $f_0$  and  $1/Q$  on  $V_g^{DC}$  are different from what is observed in nanotube resonators operated in the Coulomb blockade regime. There, the resonator experiences a reduction of  $f_0$  near the top of an oscillation in  $I^{DC}$  as a function of  $V_g^{DC}$ . In addition,  $1/Q$  is higher near the top of the oscillation in  $I^{DC}$  because electron tunneling events are accompanied by enhanced dissipation. The absence of such behaviors demonstrates that the effect of the coupling between vibrations and Coulomb blockade is weak in our experiment.

## VII. EFFECT OF ELECTROSTATIC WHITE NOISE ON THE SPECTRUM OF THE RESONATOR.

Figure 3f of the main text displays  $1/Q$  in the presence of gate voltage noise of various intensities. The gate voltage noise is applied using the Johnson-Nyquist noise of a 50 Ohm resistor at room temperature amplified by different gains (by varying the number of amplifiers). We measure the power spectral density of the amplified Johnson-Nyquist noise with a signal analyzer in a separate experiment. We verify that this amplified noise is white (the power spectral density is constant) between 1 MHz and 200 MHz, a frequency range that encompasses the resonant frequency of our resonator (40-60 MHz). Noise at frequencies below 1 MHz is cut off by a high pass filter at the sample stage. The power spectral densities we measure are consistent with the gain (20 dB) and the noise figure (1 dB) of each amplifier used in combination with the total attenuation along our radio frequency lines.

The applied Johnson-Nyquist noise creates a random electrostatic force between the nanotube and the gate (top axis of Fig. 3f). To the lowest order in the nanotube displacement,

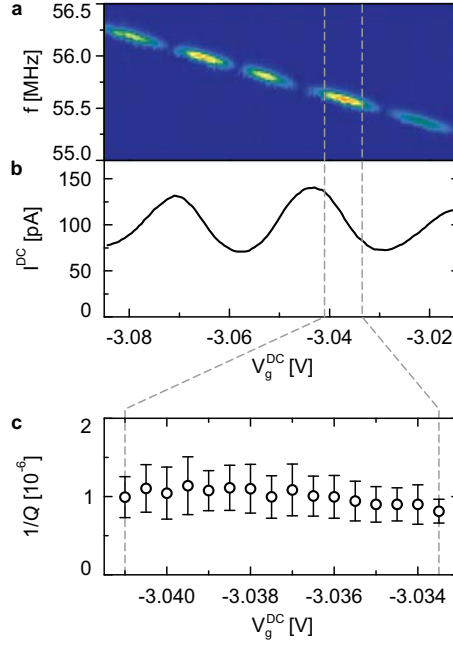


Figure S3. (a) Electro-mechanical mixing current measured with the FM technique, as a function of  $V_g^{DC}$  and drive frequency  $f$ . Scale bar from blue, 1 pA, to orange, 140 pA. (b) Source-drain DC current  $I^{DC}$  as a function of  $V_g^{DC}$ , showing Fabry-Perrot oscillations. (c)  $1/Q$  as a function of time averaged  $V_g^{DC}$ . Measurement time is 6.3 s. The error bars correspond to the distribution of  $Q$ -factors for 20 power spectra.

this force is additive, which means that it is independent of the displacement. The nanotube resonator responds primarily to the frequency components of this force, which lie within the band centered at the resonant frequency, with the typical bandwidth given by the mechanical linewidth. The power spectrum of the random force is flat in this region, and therefore the corresponding noise is white. Its intensity  $S_{ef}$  is related to the power spectral density of the Johnson-Nyquist noise  $S_{JN}$  as  $S_{ef} = (C'_g V_g^{DC} \sin \theta)^2 S_{JN}$  (see Section IV). We use  $C'_g = 5.2 \times 10^{-12}$  F/m,  $V_g^{DC} = 2.2$  V, and  $\theta = 60^\circ$ .

The effect of the additive Johnson-Nyquist noise is fully analogous to the effect of the thermal noise that comes along with the resonator dissipation. It leads to the increase of the intensity of the peak in the resonator power spectrum and to spectral broadening of this peak via nonlinear damping and via the dependence of the oscillator frequency on the vibration amplitude.

The low-frequency components of the Johnson-Nyquist noise could directly lead to fluc-

tuations of the resonator frequency, which would be similar to the low-frequency fluctuations induced by the voltage noise of the DC voltage source. They would come from the dependence of the resonator frequency on the gate voltage. Such noise is multiplicative, since the corresponding force is proportional to the resonator displacement, and this is why it acts as a frequency shift. The resonator responds to such noise if its frequencies are low, within the typical bandwidth given by the mechanical linewidth. Higher-frequency components are averaged out. For the Johnson-Nyquist noise that we are using the effect of this noise is very weak, because the initial noise from the 50 Ohm resistor is only weakly amplified below 100 kHz, and is further attenuated by a high-pass filter below 10 kHz. We estimate that the corresponding gate voltage fluctuations induce a lineshape broadening of only a fraction of a Hertz, much smaller than the linewidths we measure in Fig. 3f.

### VIII. VOLTAGE FLUCTUATIONS OF THE DC VOLTAGE SOURCES

The voltage fluctuations of both the Keithley source and of the lead battery are measured in a separate experiment. The DC source is connected to the DC gate voltage input port outside of the cryostat. A finite DC voltage close to the gate voltages used in the main text is applied. The voltage fluctuations at 300 K are measured at the sample stage after opening the cryostat. These fluctuations are recorded with a voltmeter as a function of time (Supplementary Fig. S4). The measured voltage fluctuations are larger than the intrinsic readout fluctuations of the voltmeter. These measurements are used to estimate the Allan deviation in Figs. 3c,d (blue traces) of the main text.

### IX. ADDITIONAL SAMPLE

We investigated a second nanotube resonator device operated in the Fabry-Perot regime at a refrigerator temperature of 30 mK. An example of a high  $Q$  resonance for this device is shown in Supplementary Fig. S5. The parameters used for this measurement are:  $V_g^{DC} = -3.643$  V,  $V_{sd}^{AC} = 4 \times 10^{-4}$  V, and a measurement time of 4.8 s. The measurements were carried out with the Keithley source.

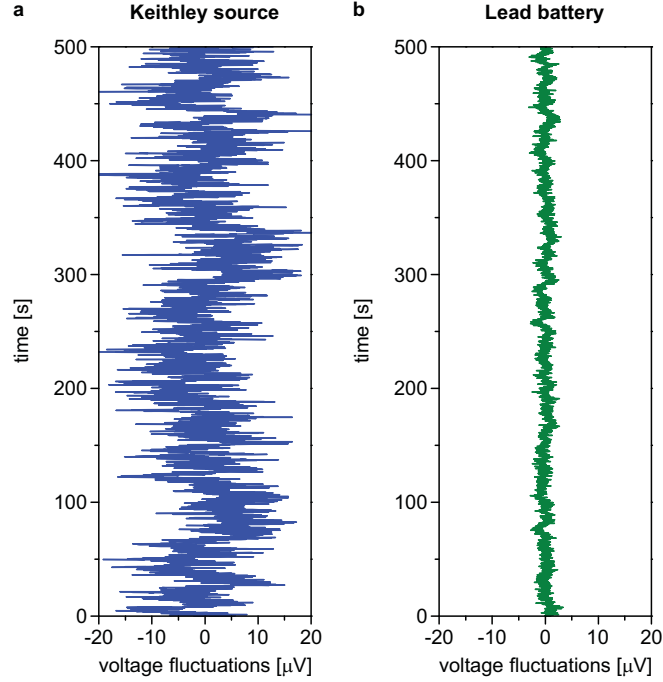


Figure S4. Gate voltage fluctuations measured at the sample stage. (a) Keithley source. (b) Lead battery.

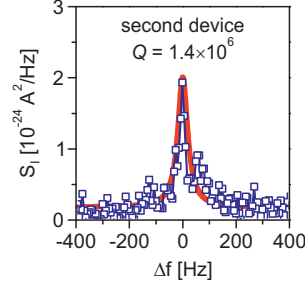


Figure S5. High  $Q$  resonance obtained with an additional device. The resonant frequency is  $f_0 \simeq 62 \times 10^6$  Hz.

## X. POWER SPECTRUM FOR A FINITE MEASUREMENT TIME

Below, power spectral densities are all *two-sided*. The power spectrum of displacement fluctuations for a finite measurement time  $\tau$  reads

$$S_q(\omega) = \frac{1}{\tau} \int_0^\tau dt \int_0^\tau dt_1 q(t)q(t_1)e^{i\omega(t-t_1)} = \frac{2}{\tau} \text{Re} \int_0^\tau dt \int_0^t dt_1 q(t)q(t_1)e^{i\omega(t-t_1)}. \quad (\text{S9})$$

We make the change from fast oscillating variables  $q(t)$ ,  $\dot{q}(t)$  to slow complex oscillator amplitude  $u(t)$

$$\begin{aligned} q(t) &= u(t)e^{i\omega_0 t} + \text{c.c.}, \\ \dot{q}(t) &= i\omega_0 (ue^{i\omega_0 t} - u^*e^{-i\omega_0 t}). \end{aligned} \quad (\text{S10})$$

Plugging Eqs. (S10) into the equation of motion  $\ddot{q} + 2\Gamma\dot{q} + [\omega_0^2 + 2\omega_0\xi(t)]q = f_T(t)/M$ , and solving for  $u$  in the rotating wave approximation, we obtain

$$u(t) = \int_{-\infty}^t dt' \exp\left[-\Gamma(t-t') + i \int_{t'}^t \xi(t'')dt''\right] f_u(t'). \quad (\text{S11})$$

In the above expression,  $\xi$  is the frequency noise,  $f_u = 1/(2iM\omega_0)f_T(t)\exp(-i\omega_0 t)$  is the thermal noise with correlator  $\langle f_u(t)f_u^*(t') \rangle = \frac{\Gamma k_B T}{M\omega_0^2}\delta(t-t')$ , and  $M$  is the modal mass. Using Eqs. (S10) and (S11) along with Eq. (S9), we obtain

$$\begin{aligned} S_q(\omega) &= \frac{2}{\tau} \text{Re} \int_0^\tau dt \int_0^t dt_1 u^*(t)u(t_1) \exp[i(\omega - \omega_0)(t - t_1)] \\ &= \frac{2}{\tau} \text{Re} \int_0^\tau dt \int_0^t dt_1 \int_{-\infty}^t dt' \int_{-\infty}^{t_1} dt'_1 \left\{ \exp[i(\omega - \omega_0)(t - t_1) - \Gamma(t - t') - \Gamma(t_1 - t'_1)] \right. \\ &\quad \left. \times \exp\left[-i \int_{t'}^t \xi(t'')dt'' + i \int_{t'_1}^{t_1} \xi(t'_1'')dt''\right] \times \frac{\Gamma k_B T}{M\omega_0^2} \delta(t' - t'_1) \right\} \\ &= \frac{\Gamma k_B T}{M\omega_0^2} \frac{2}{\tau} \text{Re} \int_0^\tau dt \int_0^t dt_1 \int_{-\infty}^{t_1} dt' \left\{ \exp[i(\omega - \omega_0)(t - t_1) - \Gamma(t + t_1 - 2t')] \right. \\ &\quad \left. \times \exp\left[-i \int_{t_1}^t \xi(t'')dt''\right] \right\} \\ &= \frac{k_B T}{M\omega_0^2} \frac{1}{\tau} \text{Re} \int_0^\tau dt \int_0^t dt_1 \exp\left[i(\omega - \omega_0)(t - t_1) - \Gamma(t - t_1) - i \int_{t_1}^t \xi(t'')dt''\right]. \end{aligned} \quad (\text{S12})$$

In Eq. (S12), we average over thermal noise since its correlation time is short on the scale  $\Gamma^{-1} \ll \tau$ . We can now separate  $\xi(t)$  into two parts, one slow and the other fast on the scale of the ring-down time  $\Gamma^{-1}$ :  $\xi(t) = \xi_{slow}(t) + \xi_{fast}(t)$ . We assume that  $\xi_{fast}$  is  $\delta$ -correlated, which allows to simplify the power spectrum in Eq. (S12) as

$$\begin{aligned} S_q(\omega) &= \frac{k_B T}{M\omega_0^2} \frac{1}{\tau} \text{Re} \int_0^\tau dt \int_0^t dt_1 \exp\left\{ \left[ i(\omega - \tilde{\omega}_0) - \tilde{\Gamma} \right] (t - t_1) - i\xi_{slow}(t)(t - t_1) \right\} \\ &= \frac{k_B T}{M\omega_0^2} \frac{1}{\tau} \int_0^\tau dt \frac{\tilde{\Gamma}}{\tilde{\Gamma}^2 + [\omega - \tilde{\omega}_0 - \xi_{slow}(t)]^2}, \quad |\omega - \omega_0| \ll \omega_0, \end{aligned} \quad (\text{S13})$$



where  $\tilde{\Gamma}$  is the “instantaneous” half-width of the spectrum and  $\tilde{\omega}_0$  is the resonant angular frequency, both renormalized by fast frequency noise. The relation between  $\Gamma$  and  $\tilde{\Gamma}$  can be found in Supplementary Ref. [4]. Equation (S13) is Eq. (2) in Methods. The resonant peak corresponding to  $S_q(\omega)$  only exists for  $\exp(-\tilde{\Gamma}\tau) \ll 1$ ; the fact that resonance lineshapes remain close to Lorentzian indicates that our measurement times exceed  $1/\tilde{\Gamma}$ .

We emphasize that  $\xi_{fast}(t)$  is  $\delta$ -correlated on the “slow” time scale  $\sim \Gamma^{-1}$ , not on the fast scale  $\sim \omega_0^{-1}$ . It is seen from Eq. (S12) that the components of  $\xi(t)$  with frequencies much higher than  $\Gamma$  are averaged out and therefore can be disregarded, as we indicated earlier. The case where the frequency noise has significant intensity near  $2\omega_0$ , so that it parametrically excites the resonator, requires a separate analysis, but we have no indications and no physical reasons to expect that strong frequency noise with frequencies  $\approx 2\omega_0$  is present in our case.

The separation of the frequency noise into parts that are slow and fast on the time scale  $1/\Gamma$  leaves out a comparatively narrow part of the noise spectrum. This part is averaged out when, as in our case, the duration of a measurement  $\tau \gg 1/\Gamma$ . It is reasonable to expect that the contribution of this narrow range of the frequency noise spectrum is small. Additional information about the spectrum of the frequency noise can be obtained by studying the power spectrum of the resonator in the presence of periodic modulation [4].

The integral width of the spectrum can be obtained from Eq. (S13). The integral width is expressed as the ratio  $\mathcal{I} = \mathcal{A}/S_q^{\max}(\omega)$ , where  $\mathcal{A} = \int_0^\infty S_q(\omega)d\omega$  is the spectrum area and  $S_q^{\max}(\omega)$  is the resonance height in the spectrum. The area  $\mathcal{A} = \pi k_B T / (M\omega_0^2)$  is independent of frequency noise or decay rate. For a Lorentzian spectrum ( $\xi_{slow} = 0$ ) we have

$$\mathcal{I}^{-1} = \frac{1}{\pi\tilde{\Gamma}} = Q \frac{2}{\pi\tilde{\omega}_0},$$

where  $Q$  is the quality factor.

Next, we calculate  $\mathcal{I}^{-1}$ , a good number to characterize  $Q$  for asymmetric and noisy resonances. For slow frequency noise of weak intensity, the expression for the reciprocal width takes on a “finite-time variance” form:

$$\mathcal{I}^{-1} \simeq \frac{1}{\pi\tilde{\Gamma}} \left( 1 - \frac{1}{\tilde{\Gamma}^2} \left[ \frac{1}{\tau} \int_0^\tau dt \xi_{slow}^2(t) - \left( \frac{1}{\tau} \int_0^\tau dt \xi_{slow}(t) \right)^2 \right] \right), \quad (\text{S14})$$

where  $\frac{1}{\tau} \int_0^\tau dt \xi_{slow}(t)$  is the measured shift of the resonant frequency resulting from slow frequency noise. The term in square brackets in Eq. (S14) is always positive, resulting in the two following effects:

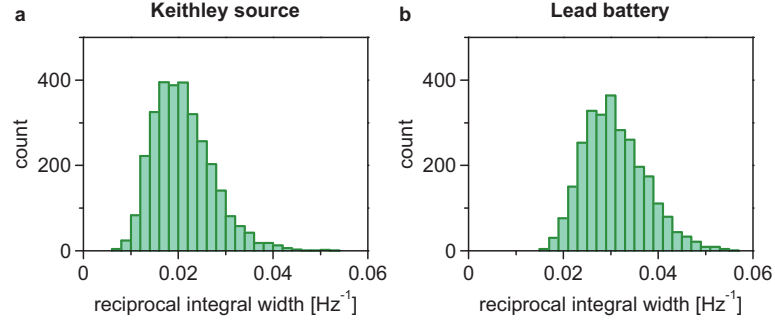


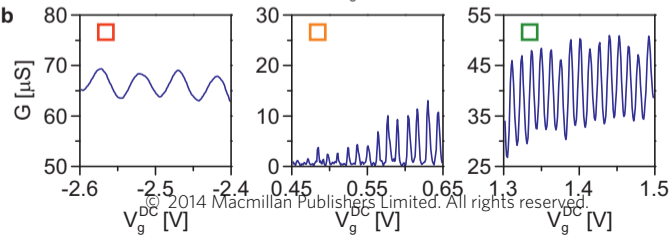
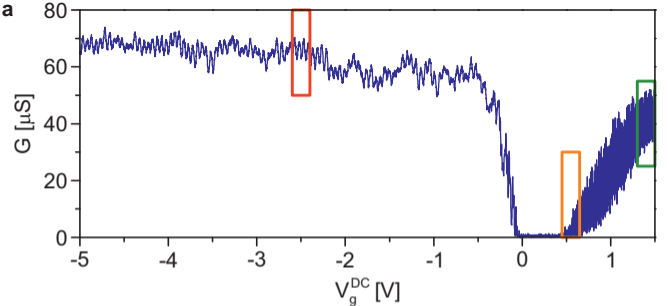
Figure S6. Histograms of the reciprocal integral width  $\mathcal{I}^{-1}$ , using the Keithley source (a) and the lead battery (b) to bias the gate electrode.

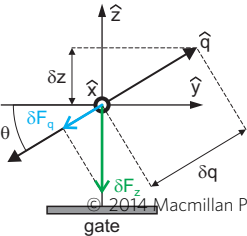
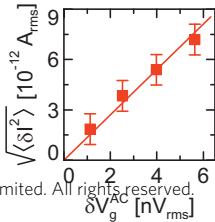
1. For a fixed measurement time  $\tau$ , multiple measurements of the integral width give an asymmetric distribution of  $\mathcal{I}^{-1}$ ;
2. As  $\tau$  increases, the peak value of the distribution of  $\mathcal{I}^{-1}$  decreases, whereas the mean  $\mathcal{I}$  increases. Once  $\tau$  exceeds the noise correlation time,  $\mathcal{I}$  levels off to the value  $\pi\tilde{\Gamma}\left(1 + \frac{1}{\tilde{\Gamma}^2}\langle\xi_{slow}^2(t)\rangle\right)$ .

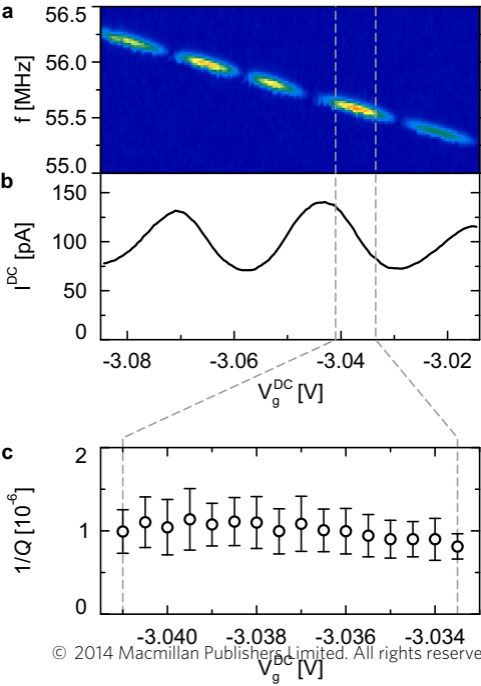
Supplementary Fig. S6 shows histograms of  $\mathcal{I}^{-1}$  built from the spectra used to construct the histograms in Figs. 2c,d of the main text. If, as we assume, the modulation of the conductance is linear in the resonator displacement, the current-to-displacement scaling coefficient drops out from  $\mathcal{I}$ . Therefore, the value of  $\mathcal{I}$  can be found directly from the data on the current power spectra. Histograms of  $\mathcal{I}^{-1}$  are asymmetric, in agreement with effect (1) predicted above. In addition, Fig. 3a of the main text shows that the peak value of the linewidth distribution tends to level off for long measurement times, in agreement with effect (2). (From that figure, we infer that the spectrum of the frequency noise has a cutoff around 1/20 Hz.) Slow fluctuations of the decay rate and/or the intensity of the thermal noise would not lead to the observed increase of the the peak value of the linewidth distribution with measurement time, but rather would cause  $\mathcal{I}$  to decrease.

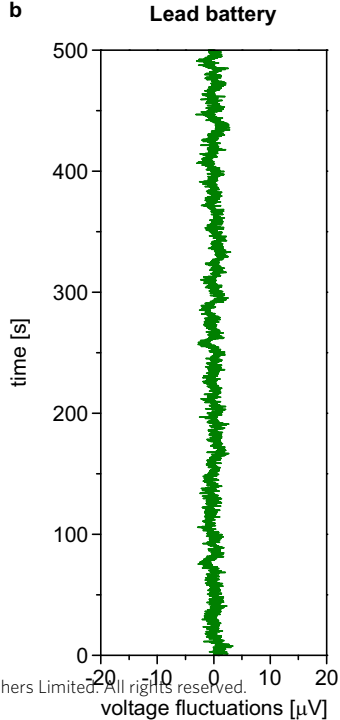
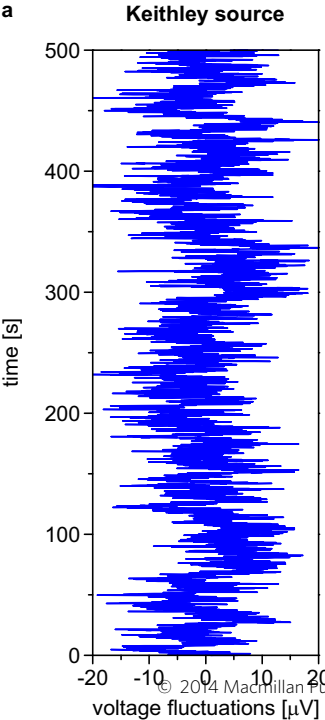
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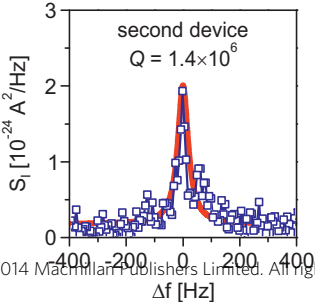
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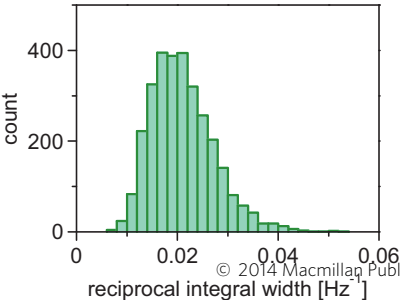
**a****b**









**a****Keithley source****b****Lead battery**